Hunting stability analysis of railway systems

Term Project in Vehicle Dynamics Course@IIT Hyderabad

Borrowed from – 'Hunting stability analysis of a railway vehicle system using a novel non-linear creep model' by Yung Chang Cheng

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What is hunting oscillation?

- Wheels of 'traction railway system' have a cone angle.
- At high speed, adhesion force is in-sufficient in maintaining stability and the wheels start to oscillate.
- This oscillation about the mean position where it is 'trying' to find the equilibrium position is called hunting.
- We pretty much know the obvious implications of these oscillation.

Approach to hunting oscillation solution

Various models

 a. Linear
 b. Non-linear

Figure 1



• A modified non-linear concept is propose by the author.

• Why linear to non-linear?

Figure 2

Cad Model of Locomotive



Cad Model of suspension system



Car Body Model

It has three parts :

- 1. Wheel
- 2. Bogie/Truck
- 3. Car



Governing equations of wheel-sets



$$m_t \ddot{y}_{ti} = F_{syti} + \left(\frac{V^2}{gR} - \phi_{se}\right) m_t g \qquad m_c \ddot{y}_c = F_{syc} + \left(\frac{V^2}{gR} - \phi_{se}\right) m_c g$$
$$m_t \ddot{z}_{ti} = F_{szti} - \left(1 + \frac{V^2}{gR} \phi_{se}\right) m_t g \qquad m_c \ddot{z}_c = F_{szc} - \left(1 + \frac{V^2}{gR} \phi_{se}\right) m_c g$$
$$I_{tx} \ddot{\phi}_{ti} = M_{sxti}$$
$$I_{tz} \ddot{\psi}_{ti} = M_{szti} \qquad I_{cx} \ddot{\phi}_c = M_{sxc}$$

Governing equations of wheel-sets

Equations for non-linear creep forces

 $m_{w}\left(\ddot{y}_{wij} - \frac{V^{2}}{R}\right) = F_{Lyij}^{n}\left(y_{wij}, \dot{y}_{wij}, \psi_{wij}, \dot{\psi}_{wij}\right)$ $+ F_{Ryij}^{n}\left(y_{wij}, \dot{y}_{wij}, \psi_{wij}, \dot{\psi}_{wij}\right)$ $+ N_{Lyij} + N_{Ryij} + F_{syij} + \frac{V^{2}}{gR}W_{ext}$ $- (W_{ext} + m_{w}g)\phi_{se}$ (27) $m_{w}\left(\ddot{z}_{wij} + \frac{V^{2}}{R}\phi_{se}\right) = F_{Lzij}^{n}\left(y_{wij}, \dot{y}_{wij}, \psi_{wij}, \dot{\psi}_{wij}\right)$ $+ F_{Rzij}^{n}\left(y_{wij}, \dot{y}_{wij}, \psi_{wij}, \dot{\psi}_{wij}\right)$ $+ N_{Rzij} + N_{Lzij} + F_{szij} - \frac{V^{2}}{gR}W_{ext}\phi_{se}$ $- (W_{ext} + m_{w}g)$ (28)

$$\begin{split} V_{wz}\ddot{\psi}_{wij} &= -I_{wy}\frac{V}{r_0}\dot{\phi}_{wij} + R_{Rxij}F_{Ryij}^n\\ &\left(y_{wij},\dot{y}_{wij},\psi_{wij},\dot{\psi}_{wij}\right)\\ &-R_{Ryij}F_{Rxij}^n(y_{wij},\dot{y}_{wij},\psi_{wij},\dot{\psi}_{wij})\\ &+R_{Lxij}F_{Lyij}^n(y_{wij},\dot{y}_{wij},\psi_{wij},\dot{\psi}_{wij})\\ &-R_{Lyij}F_{Lxij}^n(y_{wij},\dot{y}_{wij},\psi_{wij},\dot{\psi}_{wij})\\ &+\left(R_{Rxij}N_{Ryij} + R_{Lxij}N_{Lyij}\right) + M_{szij}\\ &+M_{Lzij}^n(y_{wij},\dot{y}_{wij},\psi_{wij},\dot{\psi}_{wij})\\ &+M_{Rzij}^n(y_{wij},\dot{y}_{wij},\psi_{wij},\dot{\psi}_{wij})\end{split}$$

Governing equations of wheel-sets

Equations for non-linear creep forces(Continued)

$$\begin{split} I_{wx}\ddot{\phi}_{wij} &= I_{wy}\frac{V}{r_0}\left(\dot{\psi}_{wij} - \frac{V}{R}\right) \\ &+ \left[R_{Ryij}F_{Rzij}^n(y_{wij},\dot{y}_{wij},\psi_{wij},\dot{\psi}_{wij})\right] \\ &- R_{Rzij}F_{Ryij}^n(y_{wij},\dot{y}_{wij},\psi_{wij},\dot{\psi}_{wij})\right] \\ &+ \left[R_{Lyij}F_{Lzij}^n(y_{wij},\dot{y}_{wij},\psi_{wij},\dot{\psi}_{wij})\right] \\ &+ \left[R_{Lyij}F_{Lzij}^n(y_{wij},\dot{y}_{wij},\psi_{wij},\dot{\psi}_{wij})\right] \\ &- R_{Lzij}F_{Lyij}^n(y_{wij},\dot{y}_{wij},\psi_{wij},\dot{\psi}_{wij})\right] \\ &+ \left(R_{Lyij}N_{Lzij} + R_{Ryij}N_{Rzij}\right) \\ &- \left(R_{Rzij}N_{Ryij} + R_{Lzij}N_{Lyij}\right) \\ &+ M_{Lxij}^n(y_{wij},\dot{y}_{wij},\psi_{wij},\dot{\psi}_{wij}) \\ &+ M_{Rxij}^n(y_{wij},\dot{y}_{wij},\psi_{wij},\dot{\psi}_{wij}) \\ &+ M_{sxij} + M_{exij} \end{split}$$

Assumptions

- $\alpha_{ij} = 1$
- $\phi_{wij} = (\lambda y_{ij})/a$
- $\phi_{se} = 0$
- W=W_{ext}

(to convert non-linear to linear)

(roll angle of front and rear wheels)(super-elevation angle of curved track)(external load)

Proposed linear model

$$\begin{split} m_{w}\ddot{y}_{wi} &= -\frac{2f_{11}}{V}\dot{y}_{wi} + 2f_{11}\psi_{wi} & I_{wz}\ddot{\psi}_{wi} = -\frac{2af_{33}\lambda}{r_{o}}y_{wi} + \frac{2f_{12}}{V}\dot{y}_{wi} \\ &- \frac{2f_{12}}{V}\dot{\psi}_{wi} - W\frac{\lambda}{a}y_{wi} - \frac{2r_{o}f_{11}}{V}\left(\frac{\lambda}{a}\right)\dot{y}_{wi} & + (-2f_{12} + a\lambda W)\psi_{wi} \\ &- 2K_{py}y_{wi} - 2C_{py}\dot{y}_{wi} - (-1)^{i}2K_{py}L_{1}\psi_{t} & - \left(\frac{2a^{2}f_{33}}{V} + \frac{2f_{22}}{V}\right)\psi_{wi} \\ &- (-1)^{i}2C_{py}L_{2}\dot{\psi}_{t} + 2K_{py}y_{t} + 2C_{py}\dot{y}_{t} & + \left(-\frac{I_{wy}V}{r_{o}} + \frac{2r_{o}f_{12}}{V}\right)\left(\frac{\lambda}{a}\right)\dot{y}_{wi} + M_{szi} \end{split}$$

Proposed linear model(continued)

$$M_{szti} = (-4K_{py}L_1^2 - 4K_{px}b_1^2 - 2K_{sx}b_2^2)\psi_{ti} + (-4C_{py}L_2^2 - 4C_{px}b_1^2 - 2C_{sx}b_3^2)\dot{\psi}_{ti} + 2K_{py}L_1y_{wi1} + 2C_{py}L_2\dot{y}_{wi1} + 2K_{px}b_1^2\psi_{wi1} + 2C_{px}b_1^2\dot{\psi}_{wi1} - 2K_{py}L_1y_{wi2} - 2C_{py}L_2\dot{y}_{wi2} + 2K_{px}b_1^2\psi_{wi2} + 2C_{px}b_1^2\dot{\psi}_{wi2} + 2K_{sx}b_2^2\psi_c + 2C_{sx}b_3^2\dot{\psi}_c$$

Stability Analysis using Lyapunov

• How to use it in this model?

$$\ddot{y} = a\dot{y} + by + c\psi + d\psi \dot{\psi} = A\dot{y} + By + E\dot{\psi} + D\psi$$

.

Note:

Values of constants are avoided to simplify the solutions

$$\begin{split} \dot{y} &= p\\ \dot{p} &= ap + by + cq + d\psi\\ \dot{q} &= \psi\\ \dot{q} &= Ap + By + Eq + D\psi \end{split}$$

Methodology

- Since the equations are linearized we find Eigen values
- Applying the stability conditions $\operatorname{Re}(\lambda) < 0$
- We arrive at an inequality to find the range of V_{ch} hunting Velocity
- We check the dependency of V_{ch} on K_{px} , K_{py} , K_{pz} , C_{px} , C_{py} , C_{pz}

Plots



Plots



References

• Figure1-

https://www.google.co.in/search?q=indian+railway+suspension&source=lnms&tbm=isch&sa=X&ved=0ahUKE wjskoiTqJbMAhUKjJQKHY6bCxIQ_AUIBygB&biw=1097&bih=541#imgrc=OUE5yJesFlyAeM%3A

- Figure 2- <u>https://en.wikipedia.org/wiki/Hunting_oscillation</u>
- Figure 3 & 4- Hunting stability analysis of a railway vehicle system using a novel non-linear creep model-Yung Chang Cheng

THANK YOU